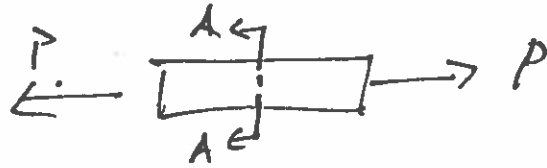


Types of stress

Lecture 7
Wednesday, October 5, 2016

Normal

From Axial Loads



$$\sigma = \frac{P}{A}$$

P : load
 A : cross section area



A-A

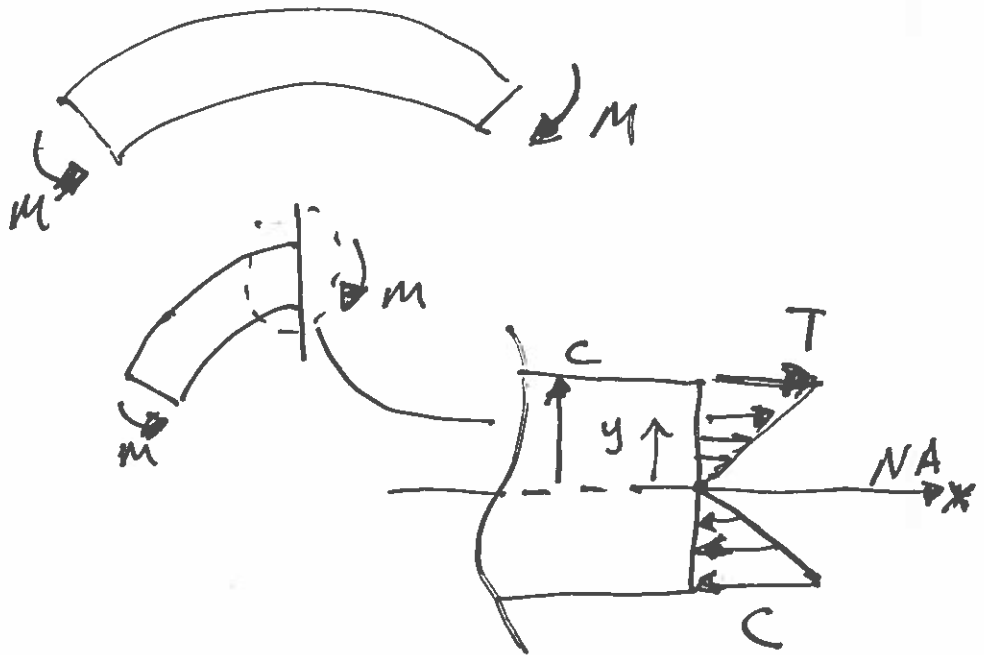
From bending

$$\sigma = \frac{My}{I}$$

M : moment

I : second moment of area

y : distance from the NA



$$\sigma_{max} = \frac{Mc}{I}$$

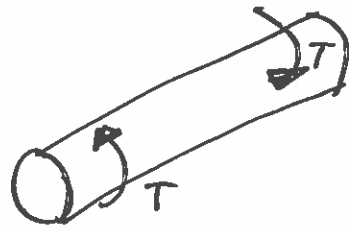
S'

See Table A-18 for common values of I and J .

Shear stresses

From torsional loads

$$\tau = \frac{Tr}{J}$$



J: polar moment of inertia

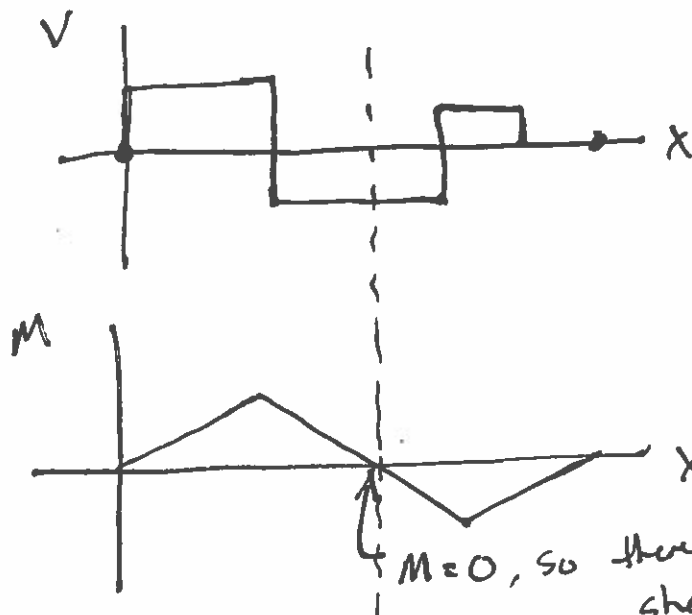
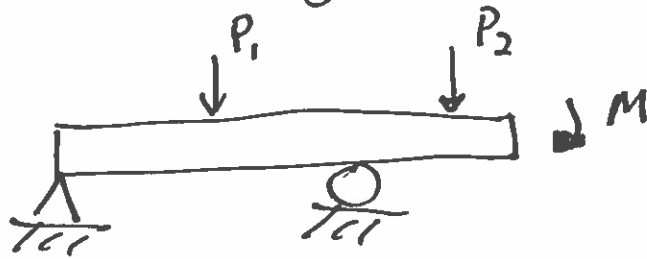
T: torque

r: radius from center

Pure Shear stress

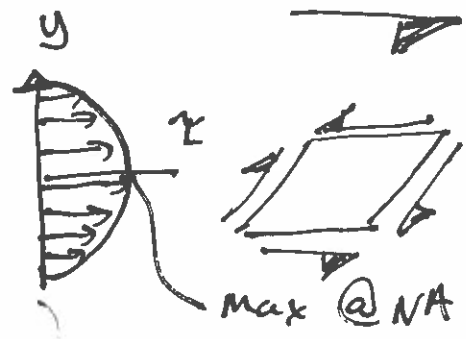
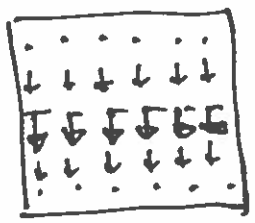
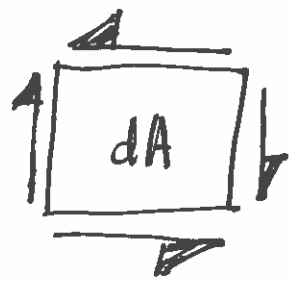
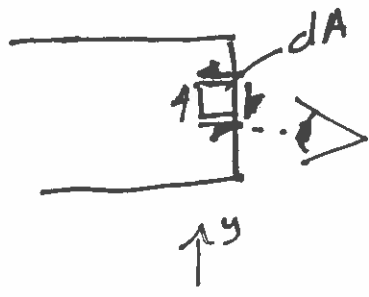
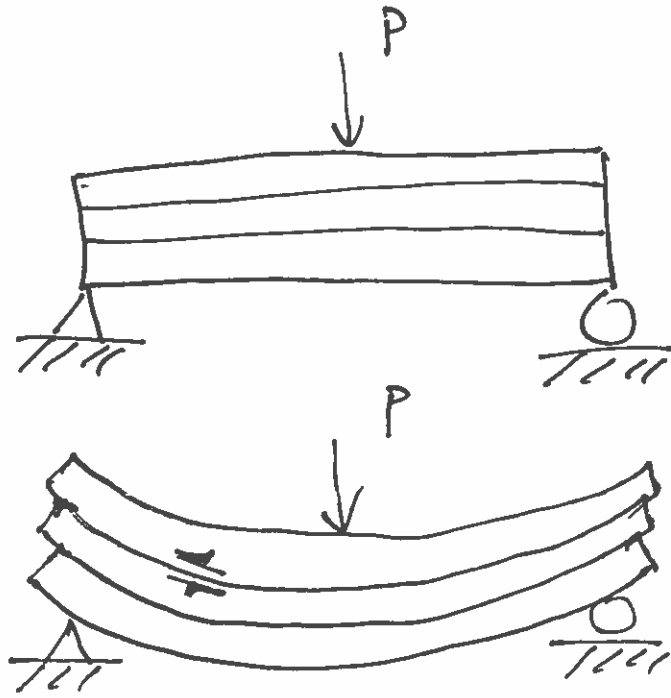
When there is no bending

$$\tau = \frac{V}{A}$$



M=0, so there is pure shear here L-7-2

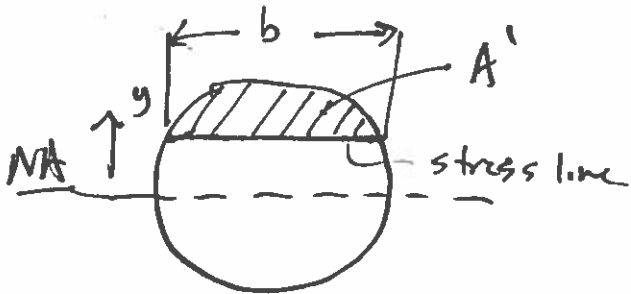
Transverse Shear



Zero at the top and bottom

shear is complementary
four shear components equal in mag

$$\tau = \frac{VQ}{Ib}$$



V: Shear force

I: Second moment of area of entire cross section

b: width at line of interest

Q: first moment of area of A'

τ is negligible for long beams

$$\left(\frac{\text{beam length}}{\text{beam height}} \gg 10 \right)$$

But shapes that have thin webs that extend far from NA may have no negligible transverse shear
eg. (I beams, channels)

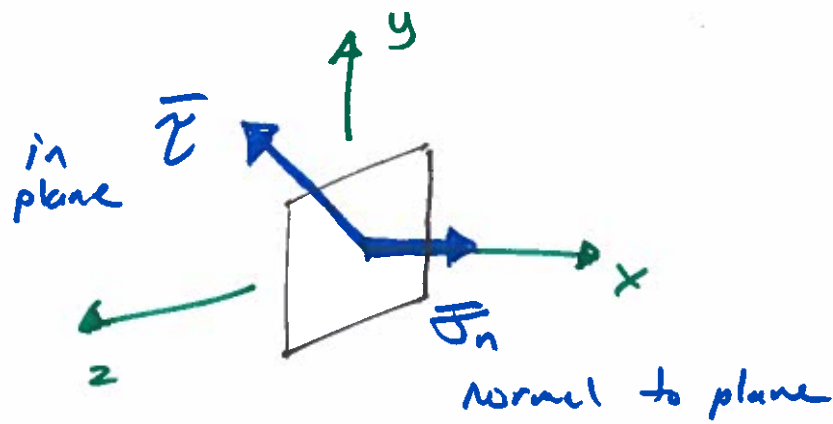
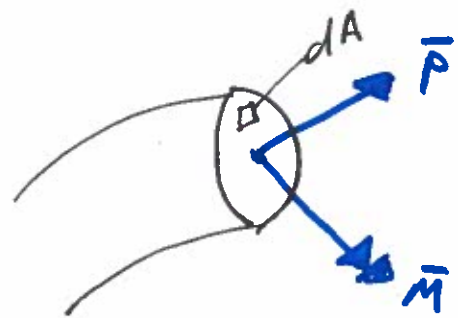
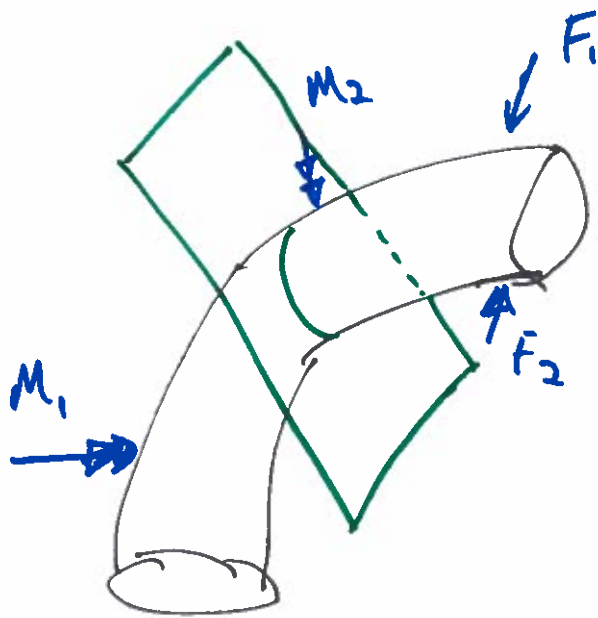
$$Q = \int y dA' = \bar{y}' A'$$

A' = cross sectional area above (or below) the stress line

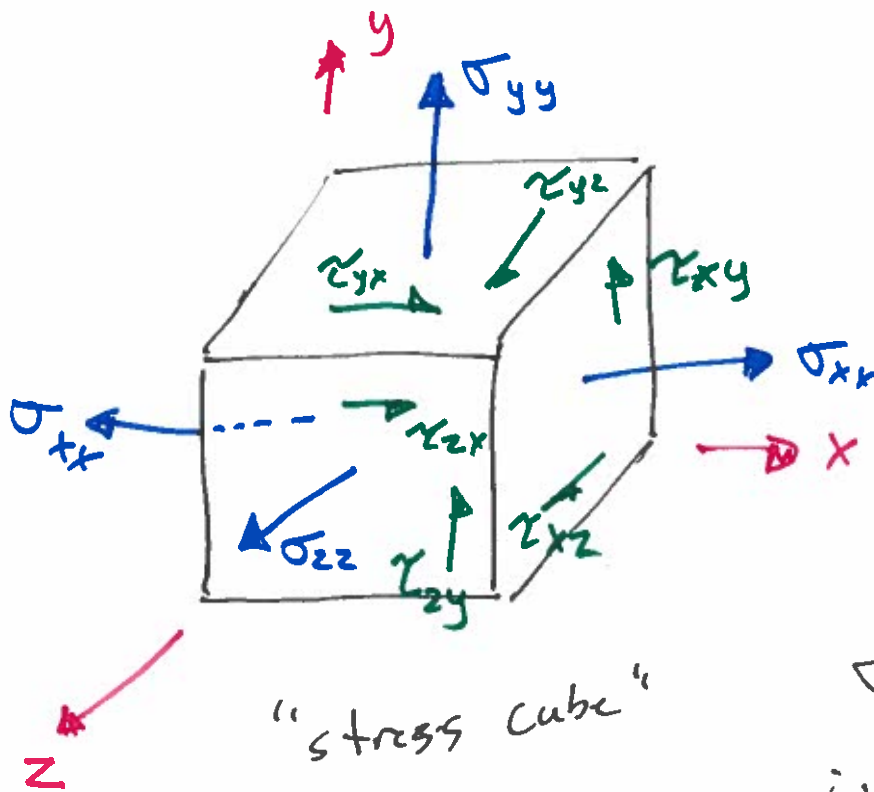
\bar{y}' = distance from the NA to centroid of A'

See table 3-2 for τ_{max} for some cross sections.

Multi-Axial Stresses



dA is a face of an infinitesimal volumetric element dV which must be in equilibrium



subscripts

$$\sigma / \tau_{ij}$$

- i : normal vector of the face
- j : direction of the stress component

- 9 components of stress
- only 6 unique values (due to complementary shear)

$$\tau_{ij} = \tau_{ji}$$